<u>Research paper</u> Design and Optimization of a Wind System Using a Genetic Algorithm

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ABSTRACT

Aims: The aim sought is to design a wind energy system can meet the energy needs of a rural household in minimizing both the economic cost and the energy cost of the system over its life cycle while ensuring continuity in the provision of electrical energy.

Study design: Design of a wind system study

Place and Duration of Study: Department of Mechanical Engineering and Energy, Laboratory Energy and Applied Mechanics, between September 2012 and March 2013.

Methodology: We have adopted an approach that requires a combination of field work and scientific work. A survey has been conducted in the locality chosen to know the equipment used to determine the consumption profile; some players were involved in determining the weight we assigned to different criteria. The NSGA-II algorithm, evolutionary genetic type was used in the context of determining the set of optimal solutions of compromise. Design variables used are the wind turbines number, batteries number, wind turbine type, battery type and height of the mast of the wind. The various programs developed have been implemented in Matlab. The method proposed has been applied to a rural household locality of Benin, named Dekin to ensure its power supply.

Results: The design made it possible to generate several candidate solutions that are available to the user. There is also the implementation of solutions and promoting the shedding of solutions providing continuous coverage of consumer needs.

Conclusion: The multi-objective design of a wind system is not an easy task since antagonistic criteria are taken into account. To this end, we found a compromise by assigning different weight goals. Solutions to economic and energy low cost are found while improving the sevice delivered to the consumer.

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Keywords: Optimization, photovoltaic autonomous, genetic algorithm, cost on life cycle, rural
 environment.

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23 **1. INTRODUCTION**

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Renewable energies account for yet only 2% in the world energy assessment, but their growth is of 30% per year **[1]**. This growth is the result of several factors: Fossil fuel depletion predictable (especially oil), impact on the greenhouse effect and other pollution (corresponding to externalities), increased taxes resulting externalities and to reduce consumption). In addition, according to industry figures BP Statistical review of world energy 2010 **[2]**, global reserves will be depleted to 2084.

31 The exhaustion of these resources associated with the climate warming which their 32 exploitation causes, must lead us to consider the development of renewable energies. 33 Among the renewable resources available in Benin, wind technology is the most 34 marginalized while studies have shown that apart from the coastal zone, there are other 35 passages that are conducive to the development of small and medium wind power. These systems also lend themselves well to a decentralized electrification especially for remote and 36 37 difficult to access. Factors that restrict the use of these systems in isolated, not connected to 38 the network are the intermittency of wind, the consumption profile uncontrollable and difficult 39 to anticipate, manage project risks and the choice of solutions that enable cover the energy 40 needs at low cost without interruption with limiting the impact on the environment. Several 41 optimization methods have been developed to deal with these types of problems. [3] have 42 proposed an optimization method to determine the optimal configuration of hybrid PV-wind. 43 This method is based on a genetic algorithm using the concept of the loss power supply 44 probability (LPSP) with a minimum annualized cost of system. [4] presented work on multi-45 objective optimization of a hybrid PV / wind / diesel / hydrogen / battery simultaneously 46 minimize the life cycle cost analysis, the CO₂ emissions related to diesel and the loss of 47 power supply probability. In this sense, a multi-objective evolutionary algorithm and genetic 48 algorithm are used to determine the optimal configuration of system components. [5] apply 49 the Pareto optimal evolutionary algorithm to perform multi-objective optimization of an autonomous PV-wind-diesel coupled to storage batteries minimizing the cost of energy and 50 51 CO₂ emissions of the life cycle of the system. They developed the hybrid optimization based 52 on Genetic Algorithms (HOGA). [6] presented a paper on the multi-objective optimization of 53 a hybrid photovoltaic-wind-diesel coupled to storage batteries. A multi-objective evolutionary 54 algorithm has been applied to minimize the life cycle cost of the system and CO₂ emissions 55 related to the use of diesel. This paper develops an optimization method which transforms 56 the multi-objective problem into a mono-objective problem using desirability functions. In this 57 study, we optimize a wind system coupled with batteries. We have proposed an optimization 58 method based on the concept of LPSP with minimization of economic cost and energy cost 59 on the system life cycle. A genetic algorithm is used to generate a set of candidate solutions 60 which will be made available to the user. Thus, the optimization method (Figure 1) adopted 61 in this study is the first to analyze the need and develop physical models of the various components and to define the evaluation criteria. Then, we determine the level of 62 63 satisfaction corresponding to the solutions and finally proceed to the evaluation and 64 classification of solutions based on the criteria.

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67 Fig. 1. Synoptic of the method of optimization used

68 Through a concrete case study, we show that optimal design is used to generate a set of 69 solutions that can help guide the choice of the decision maker.

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2. MATERIAL AND METHODS / METHODOLOGY

73 2.1 Wind turbine system

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75 The sizing system consists of wind turbines, a converter, a batteries bank, a charger and an 76 inverter. The system is autonomous, the presence of a storage device is essential in order to

- 77 satisfy, at any time, consumer demand.
- 78



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82

81 Fig. 2. Block diagram of a wind system.

83 It is intended for the power supply of a rural household of a locality of Benin (Dekin), located 84 at about thirty km of Cotonou, of Latitude 6°34'N and of Longitude 2°33'E. The consumption 85 profile adopted is shown in Figure 3. This profile is assumed to be identical for all days of the 86 year. The annual consumption is estimated at 1.523 kWh. 87



- 88
 89 Fig. 3. Distribution of the consumer power requirements during the day.
- 9091 The design variables needed to determine solutions are summarized in Table 1.
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- 97

98 Table 1. Design variables

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Design variables	Nomenclature	Range	Component type considered
Wind turbine number	N _W	1 - 20	-
Battery number	N _b	1 - 15	-
Type of wind	Tw	1 - 2	600 W 1300 W
Type of battery	T _{bat}	1 - 2	75 Ah et 100 Ah
Type of tower	T _{tower}	1 - 3	50m 60m et 70m

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101 2.2 Modeling components

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Modeling requires a set of equations characterizing all elements of the system studied. It is therefore a crucial step for the energy models of the various components must be reliable to accurately reflect the transfer of flows between different components. This stage, the condition which is essential is to know the wind speed, the profile of consumption and the relative data with the equipment, in order to be able to determine at every time, the power which the system of production can provide.

110 2.2.1 Wind turbine system model

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Power output of wind turbine generator at a specific site depends on wind speed at hub height and speed characteristics of the turbine. Wind speed at hub height can be calculated by using power-law equation [7]:

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$$V_2 = V_1 \left(\frac{Z_2}{Z_1}\right)^{\prime} \tag{1}$$

117 Where V_1 and V_2 are the wind speed at hub and reference height Z_1 and Z_2 and Γ is 118 roughness coefficient whose value generally varies between 0.1 and 0.25 depending on the 119 site. The one-seventh power law (0.14) is a good reference number for relatively flat 120 surfaces such as the open terrain of grasslands away from tall trees or buildings. The power 121 generated by the turbine is calculated as follows **[8]**:

122

123
$$P_{W} = \begin{cases} 0 ; V_{c} \leq V_{W}, V_{W} \leq V_{c} \\ P_{W\max} * \left(\frac{V_{W} - V_{c}}{V_{r} - V_{c}}\right)^{3} ; V_{c} < V_{W} \leq V_{r} \\ P_{W\max} + \frac{P_{f} - P_{W\max}}{V_{o} - V_{r}} * \left(V_{W} - V_{r}\right) ; V_{r} \leq V_{W} \leq V_{o} \end{cases}$$
(2)

124

125 Where, V_c , V_o , and V_r are the cut-in, cut-out, and rated speed of turbine (m/s), respectively. 126 Also, $P_{W \text{max}}$ is the maximum output power of the turbine (W) and P_f is the power when 127 $V_W = V_o$. The two turbines used in this study are of IMEX-Blade using Maglev technology. 128 Their characteristics are summarized in Table 9.

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132 2.2.2 Model of the storage system: charging and discharging

134 The model developed by [9] is used; which allows to calculate the storage capacity 135 depending on the power produced by the wind turbine and the load demand. Modeling of the 136 battery is necessary, particularly to establish its instantaneous state of charge with a view to 137 optimize the management of energy within the system. The state of charge of a battery at an 138 instant t, depends on its previous state (t-1). To simplify the study, we will cover the charge 139 efficiency and discharge in the overall performance of the battery (supplied energy / energy 140 consumed) we take into account the level of charge of the battery (this is ie as if the 141 discharge performance was 100%). The energy called "battery" will be an actual energy 142 available for charging [10]. The battery performance depends on several parameters 143 including fluctuates with the state of charge of the battery (depending on load current) [11]. During charging, it is between 0.65 and 0.85. Although criticized, the assumption of a 144 145 constant yield is considered in this study. Its value is taken as 85%. When the power 146 produced by the wind turbine exceeds called instantaneous power, the battery is charging 147 and capacity at time t, can be described as follows [9]:

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$$E_{B}(t) = E_{B}(t-1)(1-\dagger) + \left(E_{W}(t) - \frac{E_{L}(t)}{y_{ond}}\right) y_{bat}$$
(3)

150 When the power required by the load is greater than the energy produced by the wind 151 turbine, the battery is discharged to fill the gap, in this case, the energy stored at one 152 moment t, can be expressed by the following relation:

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$$E_B(t) = E_B(t-1)(1-\dagger) + \left(E_W(t) - \frac{E_L(t)}{y_{ond}}\right)$$
(4)

155 Where $E_B(t)$ and $E_B(t-1)$ are respectively the energy stored in the battery (Wh) at time 156 t and t-1, \dagger is the time rate of self-discharge of the battery, $E_W(t)$ is the energy 157 generated by the turbine (Wh), $E_L(t)$ is the load required (Wh), y_{ond} is the efficiency of the 158 inverter. The simulation step Δt is equal to 1h.

159160 2.2.3 Model of the inverter

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162 The power supply of the electric charges of the consumer being carried out by alternating, 163 an inverter is required to perform the DC-AC conversion. The inverter used and modeled 164 (Equation 5) has a nominal output of 2.3 kVA.

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Where, $P_{ond}(kW)$ is the power supplied by the inverter and y_{ond} the inverter efficiency.

 $P_{ond} = (P_W + P_{hat}) * y_{ond}$

(5)

169 $P_{bat}(kW)$ is the power supplied by the battery.

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171 **2.3 Criteria for evaluating system performance**

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173 **2.3.1 Definition of criteria**

The choice of criteria is a crucial step in the formulation of an optimization problem. Thus,
the criteria necessary for the evaluation of system performance is related to aspects
economic, environmental and reliability.

179 2.3.2 Models criteria

The randomness that characterizes the production system has required its analysis on all his
life. Thus, we took into account the costs of energy and economic life cycle of the system.

184 2.3.2.1 The economic model based on the LCC concept

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186 Life cycle cost (LCC) includes the cost of initial investment, the cost of replacing the 187 component, the cost of maintenance and repair and the cost of downtime. For a component 188 of the system i, the economic cost of the life cycle (during 25 years) can be expressed by 189 the following equation [12]:

$$LCC_{i} = N_{i} \left(CI_{i} + CR_{i} \cdot K_{i} + CMR_{i} \cdot PWA(ir, R_{v}) \right)$$
(6)

192 With:

193
$$K_i = \sum_{n=1}^{y_i} \frac{1}{(1+ir)^{nL_i}}$$
(7)

194
$$y_i = \left(\frac{R_v}{L_i}\right) - 1$$
 If R_v is dividable to L_i (8)

195
$$y_i = \frac{R_v}{L_i}$$
 If R_v is not dividable to L_i (9)

196
$$PWA(ir, R_{\nu}) = \frac{(1+ir)^{R_{\nu}} - 1}{ir(1+ir)^{R_{\nu}}}$$
(10)

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198 Where N_i is number/size, CI_i is the initial investment cost, CR_i is the replacement cost, 199 CMR_i is the cost of maintenance and repair of component *i*. *PWA* and K_i are annual and 200 single payment present worth factors, respectively. y_i and L_i are number of replacements 201 of component *i* and its life time. *ir* is real interest rate, R_v is project's lifetime.

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204

203 During the operating time T of the system, the energy deficit *LOEE* can be expressed by:

$$205 \qquad LOEE = \sum_{t=1}^{T} LPS(t) \Delta t \tag{11}$$

206 Where LPS(t) is the difference between the power demand and the power output of the 207 wind turbine and the battery at a time t. 208

The cost relating to the unavailability of the system during the time of simulation T can be expressed by [13]

212
$$LCC_{loss} = LOEE.C_{loss}.PWA(ir, R_v)$$
 (12)

213214 We then deduce the total economic cost of the life cycle of the system:

system. In our study, this cost is taken equal to 5.6 US\$/kWh [15].

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$$C_{total} = \sum_{i} LCC_{i} + LCC_{loss}$$
(13)

217 In this study, we chose ir = 6% and $R_v = 25$ years. The economic costs of the different

218 components of the system are summarized in Table 2.

219

220 Table 2. Components specifications ([14], [12])

221

Component	CI	CR	CMR	Efficiency (%)	Life (yr)
Wind turbine	2 US\$/W	2 US\$/W	0,02 US\$/W/yr	-	25
Battery	0,5 US\$/Wh	0,5 US\$/Wh	9 US\$/Wh/yr	85	4
Inverter	0,7 US\$/VA	0,7 US\$/VA	37 US\$/yr	90	15
Tower	250 US\$/m	250 US\$/m	6,5 US\$/m/yr	-	25

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223 2.3.2.2 Cost of Loss of Load

This cost includes all the economic consequences induced by a stop of a component or

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228 2.3.2.3 Gross energy requirement

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The life cycle analysis is a tool for decision support in eco-design for evaluating the environmental impact of the system, from raw material extraction to end of life system. The indicator chosen in this study is the Gross energy requirement (GER). This cost represents the total primary energy required for the manufacture, maintenance, recycling and transport to the place of use of the system. For an autonomous wind system, the overall energy cost is as follows:

$$GER_{Total} = N_W \cdot P_n \cdot GER_W \cdot DV_W + N_b \cdot C_{b,n} \cdot GER_{bat} \cdot y_b \cdot DV_{bat} + P_{n,inv} \cdot GER_{inv} \cdot y_{inv} \cdot DV_{inv} + GER_{tower} * H$$

$$(14)$$

Where GER_{Total} is primary energy cost of the system. GER_W is primary energy cost, P_r is rated power, DV_W is the life, of the wind. GER_{bat} is primary energy cost, DV_{bat} is the life, y_b is number of replacements, of the battery. GER_{invt} is primary energy cost, DV_{inv} is the life, y_{inv} is number of replacements, of the inverter. GER_{tower} and H are primary energy cost and height of the mast, of the wind, respectively.

244 245 2.3.2.4 Life cycle CO_2 emissions

Energy consumption during the implementation of the system generates CO₂ emissions can also be evaluated as follows:

$$GES_{Total} = N_W \cdot P_r \cdot GES_W \cdot DV_W + N_b \cdot C_{b,n} \cdot GES_{bat} \cdot y_b \cdot DV_{bat} + P_{n,inv} \cdot GES_{inv} \cdot y_{inv} \cdot DV_{inv} + GES_{tower} * H$$

$$(15)$$

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252 Where GES_{Total} is total CO₂ emissions of system, GES_W is CO₂ emission from wind, 253 GES_{bat} is CO₂ emission from battery, GES_{inv} is CO₂ emission from inverter, GES_{tower} is CO₂ 254 emission from tower.

Table 3 shows the calculation results for the energy consumption and CO₂ emissions during system equipment manufacture. These are the numerical values per unit capacity per year.

Table 3. Energy consumption and CO₂ emissions in the system equipment manufacturing ([16], [17])

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Components	Facility energy	CO ₂ emissions
Wind turbine	0,215 kWh/W.yr	69 g CO ₂ /W.yr
Battery	0,207 kWh/Wh.yr	62 g CO ₂ /Wh.yr
Inverter	0,4 kWh/VA.yr	12,5 g CO ₂ /VA.yr
Tower	7,2 kWh/m	5,9 g CO ₂ /m

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264 2.3.2.5 Loss power supply probability265

266 Because of the intermittent wind speed characteristics, which highly influence the energy 267 production from the system, power reliability analysis is usually considered as an important 268 step in any such system design process. There are a number of methods used to calculate 269 the reliability of the systems. The most popular method is the loss of power supply 270 probability (LPSP) method. The LPSP is the probability that an insufficient power supply 271 results when the system (wind power and energy storage) is not able to satisfy the load 272 demand. The design of a reliable stand-alone wind system can be pursued by using the 273 LPSP as the key design parameter. For an analysis period T, the LPSP is the ratio of the 274 sum of all values of energy loss LPS for the same period of the energy required.

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276 The loss of energy A is expressed by [9]:

$$LPS(t) = E_{L}(t) - (E_{mp}(t) + E_{B}(t-1) - E_{B,\min}) y_{ond}$$
(16)

279 *LPSP* is expressed by:

$$LPSP = \sum_{t=1}^{T} LPS(t) / \sum_{t=1}^{T} E_{L}(t)$$
(17)

(18)

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282 2.4 Models of the rates of satisfaction

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The different criteria used in this study are not the same size. To solve this problem of scaling, desirability functions for transforming the variables dimensionless criteria are tapped. But the choice of a desirability function depends on the requirements of the study to be conducted in our case, all criteria are to minimize as shown in Table 6. For this purpose, the function of desirability of Harrington is used **[18]**:

 $d(Y_{m}) = \exp(-\exp(s + r Y_{m}))$

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291 With 292

293
$$\Gamma = \frac{\ln(\ln(0.01)/\ln(0.99))}{AUC - USL}, \ S = \ln(-\ln(0.99)) - \Gamma.USL$$

Where *d* is the desirability associated with the criterion Y_m , AUC is the absolute upper cutoff, *USL* is the upper soft limit for the criterion. Levels of criteria are summarized in Table 4.

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299Table 4. Levels of criteria

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Criteria	Aim	USL	AUC	
CI	Minimize	100	70000	
CR	Minimize	100	70000	
CMR	Minimize	20	600	
LCC _{loss}	Minimize	0	10 ⁵	
LPSP	Minimize	0	60 %	
GER	Minimize	49663	2.10 ⁵	
GES	Minimize	1049968	3.10 ⁷	

301

Then, the criteria are aggregated according the aggregation method based on weighted geometric mean of the functions of desirabilities **[19]**:

304
$$DOI_k = \prod_{r=1}^q d_r^{v_r}$$
 (19)

305 Where DOI_k denote the indices of desirability and B the weights relating to the criteria.

 DOI_1 is the index relating to the economic shutter, DOI_2 is related to the reliability of the

307 system, DOI_3 is related to the environmental aspects.

308 Desirability indices obtained are aggregated according the same principle to lead to the 309 global objective function:

$$OF = \prod_{k=1}^{3} DOI_{k}^{w_{k}}$$
(20)

311 Where w_k denote the weighting coefficients concerning index of desirability.

The weights used are essential because they represent the wishes of the user in the implementation of the wind system. The values of these weights are summarized in Tables 5, 6 and 7.

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316 Table 5. Weight of the indices of desirabilities

	DOI ₁	DOI ₂	DOI ₃	
Weight (%)	22.55	67.38	10.07	

318319 Table 6. Weight-related criteria DOI₁

Criteria	CI	CR	CMR	LCC _{loss}
Weight (%)	52.24	24.93	13.4	6.79

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320

323 Table 7. Weight-related criteria DOI₃

Criteria	GER	GES
Weight (%)	62.67	37.33

327 2.5 Optimization method used

329 The optimization of the dimensioning of wind turbine system is a multi-objective optimization. 330 Indeed, the cost of the system (whether economic or energy) should be minimal while 331 providing consumers with quality electricity supply the best possible. The number of variables is important, our choice fell on a genetic algorithm called NSGA-II 332 (« Nondominated Sorting Genetic Algorithm II ») [20]. This algorithm is called evolutionary 333 334 since it refers to the theory of biological evolution. It is a multi-objective algorithm under 335 constraints, based on a comprehensive approach to optimization in the sense that the 336 exploratory nature of the algorithm will allow us to get the optimum sweeping wide spectrum 337 of possibilities offered by the range of variation of the design variables. The main parameters 338 of this algorithm are:

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- 340 Number of generations $N_G = 50$
- 341 Number of individuals per generation $N_{ind} = 100$
- 342 Design variables (table 1)
- 343 Probability of crossover $P_c = 0.80$
- 344 Mutation probability $P_m = 0.05$

The algorithm used to evaluate the performance of each individual by calculating the objectives, constraints specific to this individual and the global objective function after taking into account all the steps of the algorithm (crossover and mutation).

348 In this study, seven criteria are considered. These are:

- 349 \rightarrow Minimization of all criteria under DOI₁ (CI, CR, CMR, LCC_{loss});
- 350 \rightarrow Minimization of the criterion under DOI₂ (LPSP);
- 351 \rightarrow Minimization of all criteria under DOI₃ (GER, GES).

After modeling the problem in our approach to optimize multi-objective can be summarized as follows:

354		Find $x = [N_W, N_b, T_W, T_{bat}, T_{tower}]^T$	
355	Which minimizes	$OF(x) = \{CI(x), CR(x), \dots, GES(x)\}$	
356		Subject to $100 \le CI(x) \le 70000$	
357		$100 \le CR(x) \le 70000$	
358			
359		$1049968 \le GES(x) \le 3.10^7$	(21)
360		$1 \le N_w \le 20$	
361		$1 \le N_b \le 15$	
362		$1 \le T_W, T_{bat} \le 2$	
363		$1 \le T_{tower} \le 3$	
364			

Thus, for different sets of combination of design variables, the corresponding global
 objective functions are determined. The candidate solutions obtained are ranked in
 descending order according to their corresponding satisfaction.

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3. RESULTS AND DISCUSSION

The proposed method is applied to a wind system designed to meet the energy needs of a rural household. In Figure 8 are respectively represented the variation of the wind speed over a year.



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Fig. 8 . Variation of wind speed: (a) Speed on a Year. (b) Speed on a day to 10 m and 50 m above the ground.

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Fig.9. Evolution of the objective functions based on combinations of design variables: (a) Desirability index related to the economic shutter. (b) Desirability index related to

384 the reliability of the system.





Fig.10. Evolution of the objective functions based on combinations of design
 variables: (a) Desirability index linked to environmental aspects. (b) Global objective
 function of the system.

391 Desirability indices related respectively to economic criteria and system reliability are shown in Figure 9. We note that the maximum DOI₁ is 0.964 and the associated optimal 392 configuration corresponds to 14 wind turbines of 600 W, 3 batteries of 75 Ah with a mast 393 height of 50 m is a ratio of 0.43 Wh / W. Whereas the maximum DOI₂ is 0.9857 and the 394 optimal configuration is associated with a 600 W, 7 batteries 100 Ah, with a mast 60 m, a 395 396 ratio of 14 Wh / W. A similar representation is made in Figure 10. The maximum value DOI₃ 397 is 0.9886 and the associated optimal configuration is 9 wind turbines of 600 W, 7 batteries of 398 100 Ah with a mast 50 m, a ratio of 1.56 Wh/W. Obviously, the three indices of desirability 399 not lead to the same optimal configuration. Thus, the global objective function after 400 aggregation index of desirability and shown in Figure 10 has the maximum value 0.8284. 401



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Fig. 11. 3D for various combinations of wind turbines and batteries for different values
 of LPSP and CI.

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Figure 11 is a 3D representation of the loss power supply probability and initial investment
costs for various combinations of wind turbines and batteries with types of wind turbines,
batteries and masts fixed.





Fig.12. Sizing results for consumption profile characteristic



413 Figure 12 (a), it is possible to observe all the solutions in the plane defined by two such 414 criteria are minimized. Logically, the criteria are contradictory, more the consumer tolerates an important LPSP, the greater the wind system may be undersized and therefore cheaper 415 416 on the whole of his life. For example, the fact of tolerating an unballasting of only of 10% of 417 the energy called by the consumer makes it possible to reduce the GER of 67%. The 418 explanation is that the system is dimensioned to operate in the harshest conditions that may 419 occur on the time of use, accept a low LPSP relieves the system corresponding period. The 420 system can then be undersized.



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Table 8. Characteristics of the ten best solutions

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N°	Nw	Nb	Τw	T _{bat}	T _{tower}	CI	CR	CMR	LCC _{loss}	GER	GES	LPSP	OF
1	9	7	1	2	50	20358	20358	471	238	50190	2253783	0,8011	0,82284
2	14	3	1	2	50	17816	17816	413	232	51470	2081512	0,7809	0,8152
3	14	4	1	1	50	23816	23816	511	167	71270	4153587	0,5631	0,8147
4	13	3	1	2	60	22103	22103	502	261	84350	1052043	0,8789	0,8138
5	8	10	1	1	70	23560	23560	479	141	75750	6223240	0,4752	0,8041
6	5	8	2	2	50	25004	25004	542	181	81820	4500027	0,6077	0,8027
7	5	10	2	1	50	22003	22003	461	198	90720	3121984	0,6664	0,7991
8	9	7	1	1	50	26274	26274	541	140	89660	5190891	0,4702	0,7985
9	11	4	1	1	70	30704	30704	639	104	90500	7260086	0,3497	0,9338
10	5	13	2	1	60	22792	22792	497	198	100200	3123424	0,6659	0,7848

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The characteristics of the ten best solutions are summarized in Table 8. This table implements solutions to promote shedding solutions and ensuring continuous coverage of consumer needs. In addition, the battery bank corresponding to the tenth solution has a total nominal capacity of 975 Ah and variation of available capacity during the year is shown in Figure 12 (b).

430

431 **4. CONCLUSION**

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In this paper, we described the definition of criteria for evaluating the performance of a windsystem autonomy over its life cycle. These criteria were used for the simulation in the

435 context of optimizing the design of the system. To carry out these studies, a methodology for 436 analysis and multi-objective optimization based on conflicting criteria: cost (economic or 437 energy) of the life cycle and other quality of service associated with shedding consumption. 438 The aim of the proposed methodology is to determine from a list of components available on 439 the market, the optimal number of wind turbines, batteries and the optimal type of wind 440 turbines, batteries and mast. For each combination of sets of design variables is calculated 441 the minimum cost (economic and energy) of the system life cycle while ensuring 442 uninterrupted coverage of consumer needs. Different objective functions used in this study 443 are aggregated through weight defining the consumer wishes to obtain the global objective 444 function. The method of genetic algorithm was used to generate candidate solutions which 445 are ranked in descending order according to their corresponding objective function. The 446 proposed method has been applied to the design of a wind turbine system for the production 447 of electrical energy to a rural household.

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Characteristics	wind turbine 1	wind turbine Z	
P _{Wmax}	600 W	1300 W	
Diameter	1.06 m	2 m	
height	1.20 m	2.1 m	
V _c	1 m/s	1 m/s	
V _r	12 m/s	13 m/s	
Vo	65 m/s	60 m/s	
P _f	580 W	1200 W	

508

509	Batteries of 75 Ah and	100 Ah (only nomina	I capacity of two different)
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510

511 $U_{b,n} = 12 V$; † = 0.00004; DOD = 85%; $y_{bat} = 85\%$